# Recursive Form of the Eigensystem Realization Algorithm for System Identification

Richard W. Longman\*

Columbia University, New York, New York

and

Jer-Nan Juang†

NASA Langley Research Center, Hampton, Virginia

An algorithm is developed for recursively calculating the minimum realization of a linear system from sampled impulse response data. The Gram-Schmidt orthonormalization technique is used to generate an orthonormal basis for factorization of the data matrix. The system matrix thus identified is in upper Hessenberg form, which has advantages for the identification of modal parameters including damping coefficients, frequencies, mode shapes, and modal participation factors. It also has the property that once an element of the system matrix is computed, it is never altered as the dimension of the model is increased in the recursive process. Numerical examples are presented for comparison of the recursive and nonrecursive forms of the Eigensystem Realization Algorithm.

### Introduction

THERE is a vast body of work on linear system identification, particularly in the fields of structures and controls. In the area of system identification for flexible structures, the identification of modal parameters is a rapidly developing technology.  $^{1-10}$  Several time-domain and frequency-domain methods have been developed and successfully tested. Many different methods are, in fact, quite similar in the sense that they are mathematically equivalent, from the point of view of system realization theory<sup>2</sup> from the control field.  $^{11}$  The realization of a linear system is a triplet of matrices [A,B,C] where A is the state matrix, B is the input matrix, and C is the output matrix. The methods developed to date for identification of flexible structures are nonrecursive with only few exceptions, as in Refs. 12 and 13 that use the concept of lattice filter theory to determine the coefficients of the ARMA model. It is difficult to compute the modal parameters from the ARMA model.

The system characteristics of a large flexible structure in space can vary quickly. For example, reorientation of a large antenna on a spacecraft suddenly changes the inertia and stiffness properties. Also, sudden changes of spacecraft shape occur due to temperature gradient induced by shadowing. Attitude and shape control in such applications require real-time computation for quick update of the system model for better control performance. Real-time system identification needs a simple and fast computational procedure that is usually in a recursive form. 14,15

A simple and fast algorithm is presented for the identification of linear systems from sampled impulse response data. The algorithm, together with certain confidence criteria, represents an alternative version of the Eigensystem Realization Algorithm (ERA).<sup>2,3</sup> The standard version of ERA, which has proved valuable in the structures community for modal parameter identification from test data, operates on a large

block data matrix and truncates based on singular values to achieve the final identified model. The algorithm produced here is based on Gram-Schmidt orthonormalization, <sup>16</sup> and recursively builds up the order of the model until the appropriate order is reached. As a result, the recursive version of ERA is very efficient and requires very little storage. It automatically gives the identified system matrix in upper Hessenberg form, <sup>16</sup> which has advantages for eigensystem analysis. It has the desirable property that, given the identification results for any chosen order, the realizations for any lower-order model are immediately obtained by truncation of the system matrices. Examples are given comparing the recursive version to the standard version of ERA.

# **Background**

This section gives some mathematical background, including the continuous-time process and its sampled data, and the basic formulation of a minimum realization. The relationships of modal parameters, such as damping coefficients, natural frequencies, mode shapes, and modal participation factors, to the realized system matrices are included.

## The Continuous Process and its Sampled Data

Consider a continuous process that can be represented by finite dimensional linear time-invariant system equations in terms of the system matrices  $A_c$ , B, and C:

$$x(t) = A_c x(t) + Bu(t)$$
 (1a)

$$y(t) = Cx(t) \tag{1b}$$

If the system equations are diagonalizable, Eq. (1) can be transformed into the modal equations

$$q(t) = \Lambda q(t) + \widehat{B}u(t)$$
 (2a)

$$y(t) = \hat{C}q(t) \tag{2b}$$

where  $\Lambda = \Psi^{-1}A_c\Psi$  is diagonal,  $\Psi$  is a transformation matrix,  $\hat{B} = \Psi^{-1}B$ , and  $\hat{C} = C\Psi$ . In the structures field,  $\Lambda$  contains vibration frequencies and damping coefficients,  $\hat{B}$  and  $\hat{C}$  are called modal participation factors and mode shapes, respectively.

For purposes of identification, the impuse response for zero initial conditions  $y^{(j)}(k \Delta t) = C \exp(A_c k \Delta t)b^{(j)}$  is obtained at

Received July 27, 1987; presented at the AIAA/AAS Astrodynamics Conference, Williamsburg, VA, Aug. 18–20, 1986; revision received Nov. 4, 1987. Copyright © 1988 American Institute of Aeronautics and Astronautics, Inc. No copyright is asserted in the United States under Title 17, U.S. Code. The U.S. Government has a royalty-free license to exercise all rights under the copyright claimed herein for Governmental purposes. All other rights are reserved by the copyright owner.

<sup>\*</sup>Professor of Mechanical Engineering. Associate Fellow AIAA. †Senior Research Scientist. Associate Fellow AIAA.

sample times  $k \Delta t$ , for an impulse at t = 0 in the jth input  $u_j$ . Here  $b^{(j)}$  is the jth column of B, k is an integer, and  $\Delta t$  is the sampling time. The collection of such impulse responses obtained for all j is denoted by

$$Y(k) = C[\exp(A_c \Delta t)]^k B = CA^k B$$
 (3)

where  $A = \exp(A_c \Delta t)$ . Note that Y(0) represents data Y(0+), referring to the time instant immediately after the impulse is applied.

The realization algorithms discussed in the sequel will obtain expressions for A, B, and C, which realize the impulse response sequences according to Eq. (3). Let  $\Psi$  be chosen as the matrix that diagonalizes A, i.e.,

$$\Psi^{-1}A\Psi = \operatorname{diag}(\lambda_1, \lambda_2, \dots, \lambda_n)$$

$$= \Psi^{-1} \exp[A_c \Delta t] \Psi = \exp[(\Psi^{-1}A_c \Psi) \Delta t]$$

$$= \exp[\Lambda \Delta t]$$
(4)

The system matrices for representation (2) of the continuous system are given in terms of the B, C, and the eigenvalues and eigenvectors of A obtained in the realization algorithm, according to

$$\Lambda_k = \operatorname{diag}(\sigma_1 + i\omega_1, \dots, \sigma_n + i\omega_n) \tag{5a}$$

$$\sigma_k = \text{Re}[\ln(\lambda_k)/\Delta t] \tag{5b}$$

$$\omega_k = \operatorname{Im}[\ln(\lambda_k)/\Delta t] \tag{5c}$$

$$\hat{B} = \Psi^{-1}B \tag{5d}$$

$$\hat{C} = C\Psi \tag{5e}$$

Note that the identified matrix A can be thought of as one of the matrices of a difference equation equivalent to the continuous system (1), but because of the impulse response nature of the data, the identified B matrix is that of the continuous system (1), and *not* the usual input matrix for a discrete system that would be obtained using a zero-order hold.

# The Eigensystem Realization Algorithm

Let H(k) be the Hankel matrix

$$H(k) = \begin{bmatrix} Y(k) & Y(k+1) & \dots & Y(k+s-1) \\ Y(k+1) & Y(k+2) & \dots & Y(k+s) \\ \vdots & \vdots & \vdots & \vdots \\ Y(k+r-1) & Y(k+r) & \dots & Y(k+r+s-2) \end{bmatrix}$$

of data associated with the n-dimensional system (1), and pick r and s to be any numbers large enough that the rank of the matrix cannot be increased by increasing r and s. Then the rank of H(k) is n for all k (assuming perfect noiseless data).

Define a controllability matrix P, an observability matrix Q, and matrices  $E_{\beta}$ ,  $E_m$  according to

$$P = [B, AB, \dots, A^{s-1}B]$$
 (7a)

$$Q = [C^{T}, (CA)^{T}, \dots, (CA^{r-1})^{T}]^{T}$$
 (7b)

$$E_{\beta}^{T} = [I_{\beta}, 0_{\beta}, \dots, 0_{\beta}]^{T}$$

$$(7c)$$

$$E_m^T = [I_m, 0_m, \dots, 0_m]^T$$
 (7d)

where  $\beta$  and m are the dimensions of the measurement vector y(t) and control vector u(t), and  $I_{\beta}$ ,  $I_{m}$  are identity matrices of order  $\beta$  and m, and  $0_{\beta}$  and  $0_{m}$  are  $\beta \times \beta$  and  $m \times m$  zero matrices. Then it is clear from direct substitution that

$$Y(k) = E_R^T H(k) E_m \tag{8a}$$

$$H(k) = QA^kP \tag{8b}$$

In theory, the realization of the triplet [A,B,C] is not unique. Consider a factorization of the rank n matrix H(0) into a product of two rank n matrices

$$H(0) = QP \tag{9}$$

where Q has n columns and P has n rows. Then the first matrix of the factorization Q can represent the observability matrix, whereas the second matrix P can represent the controllability matrix for some set of state variables, representing the controllable and observable part of the system. Then the Moore-Penrose pseudoinverse  $H^{\dagger}(0)$  is given by

$$H^{\dagger}(0) = P^{\dagger}Q^{\dagger} \tag{10}$$

Because the ranks of P and Q are n,  $P^{\dagger}$  and  $Q^{\dagger}$  can be written by

$$P^{\dagger} = P^{T}(PP^{T})^{-1}, \qquad Q^{\dagger} = (Q^{T}Q)^{-1}Q^{T}$$
 (11)

Hence, combination of Eqs. (9-11) yields

$$PH^{\dagger}(0)Q = PP^{\dagger}Q^{\dagger}Q = I_n \tag{12}$$

With these mathematical preliminaries, one can obtain the following realization. Using Eqs. (8) and (11)

$$Y(k) = E_{\beta}^{T} Q A^{k} P E_{m} = E_{\beta}^{T} Q (Q^{\dagger} Q A^{k} P P^{\dagger}) P E_{m}$$
$$= E_{\beta}^{T} Q [Q^{\dagger} H (1) P^{\dagger}]^{k} P E_{m}$$
(13)

and by comparison to Eq. (3) we see that Y(k) can be realized using

$$A = Q^{\dagger}H(1)P^{\dagger}, \qquad B = PE_m, \qquad C = E_B^TQ \qquad (14)$$

Equation (14) is the basic formulation for the ERA.

One choice of the factorization in Eq. (9) is the singular value decomposition<sup>17</sup> that yields

$$H(0) = USV^T \tag{15}$$

where S is the  $n \times n$  diagonal matrix of nonzero singular values, and U and V each have n orthonormal columns of appropriate dimension. Therefore, let

$$P = S^{\frac{1}{2}}V^T, \qquad Q = US^{\frac{1}{2}}$$

Equation (14) becomes

$$A = S^{-\frac{1}{2}}U^{T}H(1)VS^{-\frac{1}{2}}, \quad B = S^{\frac{1}{2}}V^{T}E_{m}, \quad C = E_{\beta}^{T}US^{\frac{1}{2}}$$
 (16)

This is the standard version of the ERA formulation. An alternative decomposition of H(0) in Eq. (9), based on Gram-Schmidt orthonormalization, is used here to obtain desirable recursive properties for Eq. (14).

#### Discussion

The usual realization in ERA is that of Eq. (16). Since S is an  $n \times n$  matrix, then so is A, and Eq. (16) represents a minimal realization. In using this realization, one generally starts from a Hankel matrix of a significantly larger dimension than one expects for the system, and performs singular-value decomposition on this relatively large matrix in order to pick the order n of the realization.

This paper aims at generating a new version of ERA that successively increases the order of the realization until the proper order n is reached, rather than going beyond the proper order and then truncating the system based on the singular values. Such a recursive approach could have storage and computation-time advantages, although one might expect some degradation in accuracy. One would expect such a recursive algorithm to have sufficiently small computational requirements to be appropriate for use on a personal computer.

In this paper, we consider successively increasing the number of columns in the Hankel matrix, maintaining throughout a number of rows greater than the expected order of the system and greater than the number of columns treated. It is necessary to have a method of monitoring the change in the rank of the Hankel matrix as columns are added. Then, when the rank no longer increases, one has arrived at the system order n. We choose to do this using a Gram-Schmidt orthonormalization.

### Recursive Orthonormalization and the Pseudoinverse

This section develops certain mathematical results used to generate the identification algorithm. The recursion considered here uses a Hankel matrix with a fixed number of rows, and increases the number of columns one by one. Introduce a single subscripted notation  $H_i$ , where j denotes the number of columns (which need not be equivalent to an integer number of column partitions). Let the columns of  $H_i$  be  $h_i$  so that

$$H_j = [h_1, h_2, \dots, h_j]$$
 (17)

Known properties of the Hankel matrix<sup>11</sup> indicate that when the columns represent noiseless measurements of the impulse response of an *n*th order realization, Eq. (3), the  $h_i$  for  $i = 1, 2, \dots, n$ , will be linearly independent, but all  $h_i$  for i > ncan be written as a linear combination of the first n columns.

The Gram-Schmidt orthonormalization of the columns of  $H_i$ produces a matrix of orthonormal columns, spanning the same space, according to

$$\hat{H}_i = [\hat{h}_1, \hat{h}_2, \dots, \hat{h}_i] \tag{18a}$$

$$\bar{h_i} = h_i - \sum_{k=1}^{i-1} (h_i^T \hat{h_k}) \hat{h_k}$$
 (18b)

$$\hat{h}_i = \bar{h}_i / |\bar{h}_i| \tag{18c}$$

$$i = 1, 2, 3, \dots, j$$
 (18d)

Statement:

1) Matrix  $\hat{H}_i$  can be expressed in the form

$$\hat{H}_j = H_j \Phi_j \tag{19}$$

where  $\Phi_i$  is a  $j \times j$  upper triangular matrix.

2) Expression (19) can be recursively computed as j increases using the following formulations:

$$\Phi_1 = 1/|h_1|, \qquad \hat{H}_1 = h_1/|h_1|$$
 (20a)

$$\bar{h}_{j+1} = h_{j+1} - \hat{H}_j(\hat{H}_j^T h_{j+1}) \tag{20b}$$

$$\Phi_{j+1} = \begin{bmatrix} \Phi_j & -\Phi_j \hat{H}_j^T h_{j+1} / |h_{j+1}| \\ 0 & 1 / |h_{j+1}| \end{bmatrix}$$
 (20c)

$$\hat{h}_{j+1} = \bar{h}_{j+1}/|\bar{h}_{j+1}| \tag{20d}$$

$$\hat{H}_{i+1} = [\hat{H}_i, \hat{h}_{i+1}], \qquad j = 1, 2, 3, \dots, n-1$$
 (20e)

where the recursion ends when the number of columns reaches the order n of the system, after which all additional columns are linearly dependent on  $\bar{h}_1, \bar{h}_2, \ldots, \bar{h}_n$  and  $|\bar{h}_{n+1}| = 0$ .

3) Matrix  $\hat{H}_i$  can be decomposed into the following form:

$$H_i = \hat{H}_i \Gamma_i \tag{21a}$$

$$\Gamma_{j} = \begin{bmatrix} |\bar{h}_{1}| & h_{2}^{T}\bar{h}_{1} & \dots & h_{j}^{T}\bar{h}_{1} \\ 0 & |\bar{h}_{2}| & \dots & h_{j}^{T}\bar{h}_{2} \\ \vdots & & & \vdots \\ 0 & 0 & \dots & |\bar{h}_{j}| \end{bmatrix}$$
(21b)

where  $\Phi_i = \Gamma_i^{-1}$ .

*Proof:* The sequential operations of Gram-Schmidt can be written in the form

$$[\hat{h}_1, h_2, \dots, h_j] = [h_1, h_2, \dots, h_j] \phi_1 D_1$$

$$[\hat{h}_1, \hat{h}_2, h_3, \dots, h_j] = [\hat{h}_1, h_2, \dots, h_j] \phi_2 D_2$$

$$[\hat{h}_1, \hat{h}_2, \hat{h}_3, h_4, \dots, h_j] = [\hat{h}_1, \hat{h}_2, h_3, \dots, h_j] \phi_3 D_3$$

$$\hat{H}_i = H_i[\phi_1 D_1, \phi_2 D_2, \phi_2 D_3, \dots, \phi_j D_j] = H_i \Phi_i$$

where

$$\phi_1 = I_i, \qquad D_1 = \text{diag}(1/|h_1|, I_{i-1})$$
 (22a)

$$D_k = \text{diag}(I_{k-1}, 1/|\bar{h}_k|, I_{i-k})$$
 (22b)

$$\phi_k = I_i - C_k \tag{22c}$$

Here  $C_k$  is the  $j \times j$  zero matrix with the kth column replaced

$$[h_k^T \hat{H}_{k-1}, 0, \dots, 0]^T = [h_k^T \hat{h}_1, h_k^T \hat{h}_2, \dots, h_k^T \hat{h}_{k-1}, 0, \dots, 0]^T$$

Hence

$$\Phi_j = \phi_1 D_1 \dots \phi_j D_j \tag{23}$$

is the product of upper triangular matrices and is, therefore, upper triangular.

Assuming that the  $j \times j$  matrix  $\Phi_j$  has been found, then the above expressions can be used to obtain the  $(j+1) \times (j+1)$ matrix  $\Phi_{i+1}$  according to

$$\Phi_{j+1} = \operatorname{diag}(\Phi_{j}, 1)\phi_{j+1}D_{j+1}$$

$$= \operatorname{diag}(\Phi_{j}, 1)[I_{j+1} - C_{j+1}] \operatorname{diag}[I_{j}, 1/|h_{j+1}|)$$
(24)

where  $\phi_{j+1}$ ,  $D_{j+2}$ , and  $C_{j+1}$  are the matrices obtained from Eq. (22), with j replaced by j+1. Then  $C_{j+1}$  becomes the  $(j+1) \times (j+1)$  zero matrix, with the last column replaced by  $[h_{j+1}^T \hat{H}_j, 0]^T$ . Performing the product in Eq. (24) produces the  $\Phi_{j+1}$  of Eq. (20). To establish part 3, note that from Eq. (23)

$$\Gamma_i = \Phi_i^{-1} = D_i^{-1} \phi_i^{-1} \dots D_1^{-1} \phi_1^{-1}$$

and that a matrix of the form  $\phi_k$  has as its inverse

$$\phi_k^{-1} = I_i + C_k$$

that is readily verified from  $(I_i + C_k)(I_i - C_k) = I_i$  since  $C_k^2 = 0$ .

# **Recursive Realization Algorithm**

Using the notation of the previous section, replace the H(0)of Eq. (6) by  $H_j$ , and distinguish this Hankel matrix from a shifted version  $H_i^{\tau}$  used in place of H(1). For simplicity we consider the case of a scalar control, so that m = 1, in which case

$$H_{j+1} = [h_1, h_1, \dots, h_j, h_{j+1}] = [H_j, h_{j+1}]$$
 (25a)

$$H_{i+1}^{\tau} = [h_2, h_3, \dots, h_{i+1}, h_{i+2}] = [H_i^{\tau}, h_{i+2}]$$
 (25b)

Let  $P = \Gamma_n$  and  $Q = \hat{H}_n$  from Eq. (14), and note that  $P^{\dagger} = \Phi_n$  and  $Q^{\dagger} = \hat{H}_n^T$ , the sequence Y(k) can be realized using system matrices

$$A = \hat{H}_n^T H_n^{\tau} \Phi_n, \qquad B = \Gamma_n E_1, \qquad C = E_{\beta}^T \hat{H}_n \quad (26)$$

The recursive form of A for this realization is obtained from

$$A_{i+1} = [H_i, h_{i+1}]^T [H_i^{\tau}, h_{i+2}] \Phi_{i+1}$$

Using Eq. (20) gives

$$A_{j+1} = \begin{bmatrix} A_j & 0 \\ 0 & 0 \end{bmatrix} + \begin{bmatrix} 0 & \Delta A_{j2} \\ \Delta A_{i3} & \Delta A_{j4} \end{bmatrix}$$
 (27)

where

$$\begin{split} \Delta A_{j2} &= (\hat{H}_{j}^{T} h_{j+2} - A_{j} \hat{H}_{j}^{T} h_{j+1}) / |\bar{h}_{j+1}| \\ \Delta A_{j3} &= \hat{h}_{j+1}^{T} H_{j}^{\tau} \Phi_{j} = [0,0,\ldots,0,\hat{h}_{j+1}^{T} h_{j+1} / |\bar{h}_{j}|] \\ \Delta A_{j4} &= \hat{h}_{j+1}^{T} [h_{j+2} - H_{j}^{\tau} \Phi_{j} \hat{H}_{j}^{T} h_{j+1}] / |\bar{h}_{j+1}| \\ &= [\hat{h}_{j+1}^{T} h_{j+2} - \Delta A_{j3} \hat{H}_{j}^{T} h_{j+1}] / |\bar{h}_{j+1}| \end{split}$$

The dimensions of  $A_j$ ,  $\Delta A_{j2}$ ,  $\Delta A_{j3}$ , and  $\Delta A_{j4}$  are, respectively,  $j \times j$ ,  $j \times 1$ ,  $1 \times j$ , and  $1 \times 1$ . Note that  $\Delta A_{j3}$  takes on a particularly simple form because, by construction,  $\hat{h}_{i+1}$  is orthogonal to  $h_1, \ldots, h_i$ . The matrices B and C come from

$$C_{j+1} = [C_j, E_{\beta}^T \hat{h}_{j+1}], \qquad B_{j+1} = [|\bar{h}_1|, 0, \dots, 0]$$
 (28)

where there are j zero elements in  $B_{j+1}$ . To summarize the recursive algorithm, start with

$$\hat{H}_1 = h_1/|h_1|, \qquad A_1 = \hat{h}_1^T h_2/|h_1|$$

Use the next column of the Hankel matrix  $h_{j+1}$  and the formulas in Eq. (20) to obtain  $|\vec{h}_{j+1}|$ ,  $\hat{h}_{j+1}$ , and  $\hat{H}_{j+1}^{j+1}$ . Equations (27) and (28) then produce  $A_{j+1}$ ,  $B_{j+1}$ , and  $C_{j+1}$ . Note that there is no need for an explicit computation of  $\Phi_{j+1}$ , and that the only quantity that needs to be stored during the computation, besides the model produced, is  $\hat{H}_i$ . The most time-consuming computation is that of the matrix product  $\hat{H}_{j}^{T}h_{j+2}$  in the  $\Delta A_{j2}$ of Eq. (27), and storing it allows one to obtain easily the  $\hat{H}_{j+1}^T h_{j+2}$  of the  $\bar{h}_{j+2}$  computation, and the  $\Delta A_{(j+1)2}$  computation. tation at step j + 1. At each step j, a decision must be made as to whether appending column  $h_{j+1}$  to the Hankel matrix  $H_j$  to produce  $H_{j+1}$  has increased the rank of the matrix. If not, the current value of j is the dimension n of the realization. In the no-noise case, this situation is recognized by having  $|\overline{h}_{j+1}| = 0$ . When noise is present, the size of  $|h_{i+1}|$ , which is generally in descending order, is used to make a judgment about the proper order n of the model. Once  $A_n$ ,  $B_n$ ,  $C_n$  are determined, the continuous time realization (2) is obtained by finding the eigenvalues  $\lambda_k$  of  $A_n$ , and the matrix of eigenvectors  $\Psi$  of  $A_n$ , and using these in Eq. (5).

This algorithm has the following desirable properties:

- 1) Once an element of the  $A_i$  and  $C_i$  matrices is computed, it is never altered as the dimension of the model is increased from j to j + 1; in addition, the nonzero element of  $B_i$  is fixed for all j.
- 2) The algorithm is extremely fast and simple, requiring only a few inner products and a couple of matrix products at
- 3) At each step j, only j + 2 scalars are computed and appended to  $A_j$  to produce  $A_{j+1}$ , and only  $\beta$  scalars are computed and appended to  $C_j$  to produce  $C_{j+1}$ . Therefore, the number of computations required grows relatively slowly with the order
- 4) When significant noise is present in the data, there can be some ambiguity concerning the proper choice of the realization order n. Given the realization for a value of n, the special structure of this recursive algorithm mentioned in item 3 allows one to obtain all lower-order realizations immediately by truncation of rows and columns.
- 5) The algorithm is recursive, requiring knowledge of only  $\hat{H}_i$  and the next two columns of data in the Hankel matrix, in order to obtain the model of order j + 1 from that of order j. There is no need to compute or store any auxiliary matrices
- 6) Because of the zero elements of  $\Delta A_{j3}$  in Eq. (29), the identified system matrix  $A_n$  is in upper Hessenberg form. This

special form allows one to use particularly efficient eigenvalue and eigenvector routines to obtain the continuous system realization, Eq. (2).

- 7) Let us repeat here the original purpose of generating a recursive algorithm. The recursion allows one to increase the order of the model until the proper order is reached, rather than starting from a much larger dimension matrix and then decreasing the order to that of the system. This offers savings in computer storage and time in comparison to the more usual ERA realization. To accomplish this, and obtain the other desirable properties listed above, we have abandoned the use of singular value decomposition in favor of a Gram-Schmidt procedure, and one therefore expects some degradation in numerical sensitivity to noise.
- 8) Another recursive algorithm is derived in the Appendix using a similar approach, but it does not exhibit some of the above desirable features including items 1 and 6.

# **Numerical Examples**

Measurement data for a four-mode system were simulated using additive random noise, and then the recursive algorithm (ERA-RC) developed here was used to identify the system modes. The standard ERA algorithm using Eq. (16) was also used on the data and the results compared.

The simulated data were constructed from

$$Y(k) = \sum_{j=1}^{N} a_j \exp(-\zeta_j \Omega_j t) \cos(\omega_j \tau - \theta_j) + n(t)$$

where the parameter choices are given in Table 1; N, the number of modes, is 4,  $a_i$  are their amplitudes,  $\zeta_i$  are the damping

Table 1 Parameters used for simulation<sup>a</sup>

Mode number	Frequency, Hz	Damping ratio, %	Amplitude	Phase
1	1.0	1.0	1.0	0
2	2.0	2.0	1.0	0
3	3.0	3.0	1.0	0
4	4.0	4.0	1.0	0

a Sampling rate: 10 Hz.

Noise: uniformly distributed, white. Noise level = 10% of signal level (ratio of standard deviations). Sample mean value  $5.86 \times 10^{-3}$ . Sample standard deviation 0.0982.

Signal: Mean value of first 40 data points  $3.57 \times 10^{-2}$ . Standard deviation of first 40 data points 1.01.

Table 2 Identification results

	Mode number	Frequency, Hz	Damping ratio, %	Accuracy indicator, %
	. ,	Case 1		
	1	0.985	1.38	99.2
ERA-RC	2	1.986	2.68	99.3
	2 3	2.981	2.99	98.5
	4	4.022	3.57	98.5
	1	0.996	0.88	99.9
		1.996	1.76	99.9
ERA	2 3	3.001	2.67	99.9
	4	4.025	3.83	99.6
		Case 2		
	1	1.004	0.71	99.2
	2	2.014	2.13	98.1
ERA-RC	1 2 3	3.008	3.32	98.4
	4	3.850	4.96	82.8
	1	1.004	1.00	98.8
	2	2.011	1.61	97.8
ERA	3	3.016	6.38	92.2
	4	3.922	2.48	89.2

ratios,  $\omega_j = 2\pi f_j$  where the  $f_j$  are the frequencies in Hz,  $\theta_j$  are the phase angles taken as zero for all modes, and  $\Omega_j = \omega_j/(1-\zeta_j^2)^2$ . The n(t) is the random noise taken as uniformly distributed [-1,1] and white, with a noise level of approximately 10%, measured as a ratio of the noise standard deviation to the standard deviation of the signal for the data time steps used in the identification.

The first identification problem considered used a  $20 \times 20$  symmetric square Hankel matrix. The identification results for a 20th-order realization were identical (at least to the seven digits of the printout) for the ERA and for the recursive algorithm ERA-RC. However, a nonsymmetric  $20 \times 20$  Hankel matrix, obtained by skipping every two out of three rows, was found to produce different results.

Table 2 gives the results in two additional cases. Case 1 starts with a 20 × 20 Hankel matrix and produces an eighth-order model. In the case of ERA-RC, this is done by recursively including columns 1-8 of the Hankel matrix, and for ERA the full 20 × 20 Hankel matrix was used, and all but the first eight singular values were replaced by zeros. Comparison of the identification results with the correct values given in Table 1 shows that for some of the numbers the ERA-RC gave better results, and for others ERA was better. As a general rule, one would expect that the singular value decomposition is numerically more stable than the Gram-Schmidt orthonormalization. Therefore, the ERA results are somewhat closer to the true values, but the difference is not large. The accuracy indicator listed is the output matrix coherence (modal amplitude coherence) described in Refs. 2 and 3. It is a scalar measure of the similarity between the modal amplitude history from the data, and the modal amplitude history generated by the model.

Experience has shown that better results are often obtained when the model order is larger than the true model, since there is a tendency for the noise to contribute to the extra "modes" of the model, resulting in less noise contamination of the true modes. Case 2 in Table 2 produces an identified system matrix that is  $16 \times 16$ , allowing four extra modes for the noise. The results are seen to be significantly closer to the true values, and ERA-RC is seen to compare quite favorably with ERA. There is an additional difference in the computation for Case 2. It uses a Hankel matrix that includes only every third row of the original Hankel matrix, but is still  $20 \times 20$  in dimension.

The results of these numerical examples suggest that the recursive version of ERA is quite fast and simple, uses very little storage, and produces results with an accuracy approaching that of the standard ERA.

# **Concluding Remarks**

In general, the appropriate order for the system model is unknown. The recursive algorithm developed here allows one to build up to the proper order. In constrast, the standard version of the ERA creates a large dimensional order and then truncates to the appropriate dimension. Recursive procedures may require more computation than their nonrecursive counterparts. However, this algorithm has no loss in computational efficiency, because once the matrix elements of a realization have been computed, they will never be altered in the following recursive steps. The computations also take advantage of the special Hessenberg structure of the system matrix. The recursive form will produce the results somewhat quicker than the nonrecursive version. Future work will be directed toward the recursive identification with arbitrary forcing inputs, and will consider recursion in both columns and rows.

## **Appendix: Alternative Recursive Realization**

Another recursive implementation of Eq. (14) is derived here. When the Hankel matrix is being extended successively column by column, while the rank is being monitored, one then stops the recursion when the right number of columns n is reached to produce a minimal order realization. Let P = I and

 $Q = H_n$  in Eq. (9). It is immediately seen that Y(k) can be realized using Eq. (14)

$$A = H_n^{\dagger} H_n^{\tau}$$
  $B = E_m$ ,  $C = E_{\beta}^T H_n$  (A1)

Statement: For all  $H_j$ , j = 1, 2, ..., n, the pseudoinverse  $H_j^{\dagger} = (H_j^T H_j)^{-1} H_j$  of the full rank matrix  $H_j$  can be written as

$$H_i^{\dagger} = \Phi_i H_i^T \tag{A2}$$

Proof: The proof is trivial by making use of Eq. (21), that is

$$\begin{split} H_j^{\dagger} &= (\Gamma_j^T \hat{H}_j^T \hat{H}_j \Gamma_j)^{-1} \Gamma_j^T \hat{H}_j \\ &= (\Gamma_j^T \Gamma_j)^{-1} \Gamma_j^T \hat{H}_j \\ &= \Gamma_i^{-1} \hat{H}_i^T = \Phi_i H_i^T \end{split}$$

Let us generate a recursive calculation of the realization in Eq. (A1). The identified B and C of realization (A1) are immediately available

$$B = E_m = E_1, C = E_B^T H_n (A3)$$

and the system matrix A can be written as follows, making use of Eqs. (A1), (A2), (20), and (25):

$$\begin{split} A_{j+1} &= H_{j+1}^{\dagger} H_{j+1}^{\tau} = \Phi_{j+1} H_{j+1}^{T} H_{j+1}^{\tau} \\ &= \begin{bmatrix} \Phi_{j+1} & -\Phi_{j} \hat{H}_{j}^{T} h_{j+1} / |h_{j+1}| \\ 0 & 1 / |h_{j+1}| \end{bmatrix} \begin{bmatrix} \hat{H}_{j}^{T} \\ \hat{h}_{j+1}^{T} \end{bmatrix} \begin{bmatrix} H_{j}^{\tau} h_{j+2} \end{bmatrix} \\ &= \begin{bmatrix} A_{j} & 0 \\ 0 & 0 \end{bmatrix} + \begin{bmatrix} \Delta A_{j1} & \Delta A_{j2} \\ \Delta A_{j3} & \Delta A_{j4} \end{bmatrix} \end{split}$$
(A4)

where

$$\Delta A_{j1} = -\Phi_{j} \hat{H}_{j}^{T} h_{j+1} \hat{h}_{j+1} H_{j}^{\tau} / |\bar{h}_{j+1}|$$

$$\Delta A_{j2} = \Phi_{j} \hat{H}_{j}^{T} [h_{j+2} - h_{j+1} \hat{h}_{j+1}^{T} h_{j+2} / |\bar{h}_{j+1}|]$$

$$\Delta A_{j3} = \hat{h}_{j+1}^{T} H_{j}^{\tau} / |\bar{h}_{j+1}|$$

$$\Delta A_{j4} = \hat{h}_{j+1}^{T} h_{j+2} / |\bar{h}_{j+1}|$$

The recursion uses Eqs. (20) and (19) to obtain  $\Phi_j$ ,  $\hat{H}_j$  starting from the  $\Phi_1$ , and  $\hat{H}_1$  in Eq. (20), and then compute  $A_{j+1}$  from Eq. (A4) starting with  $A_1 = \hat{h}_1^T h_2 / |h_1|$ . The recursive realization, Eqs. (27) and (28), is preferred over this alternative realization for two reasons: the nonzero  $\Delta A_{j1}$  at each step destroys the Hessenberg form, and a lower-order model cannot be obtained immediately by truncating the last columns and rows.

#### References

1"Identification of Large Space Structures on Orbit," AFRPL Rept., Wright-Patterson AFB, OH, Aug. 1986.

<sup>2</sup>Juang, J. N., "Mathematical Correlation of Modal Parameter Identification Methods via System Realization Theory," *The International Journal of Analytical and Experimental Modal Analysis*, Vol. 2, Jan. 1987, pp. 1–18.

<sup>3</sup>Juang, J. N. and Pappa, R. S., "An Eigensystem Realization Algorithm (ERA) for Modal Parameter Identification and Model Reduction," *Journal of Guidance, Control, and Dynamics*, Vol. 8, Sept.—Oct. 1985, pp. 620–627.

<sup>4</sup>Juang, J. N. and Pappa, R. S., "Effects of Noise on Modal Parameters Identified by the Eigensystem Realization Algorithm," *Journal of Guidance, Control, and Dynamics*, Vol. 9, May–June 1986, pp. 620–627.

<sup>5</sup>Vold, H., Kundrat, J., Rocklin, G. T., and Russell, R., "A Multi-Input Modal Estimation Algorithm for Mini-Computers," Society of Automotive Engineers, Paper 820194, Feb. 1982.

<sup>6</sup>Vold, H. and Russell, R., "Advanced Analysis Methods Improve Modal Test Results," *Sound and Vibration*, March 1983, pp. 36–40.

<sup>7</sup>Juang, J. N. and Suzuki, H., "An Eigensystem Realization Al-

gorithm in Frequency Domain for Modal Parameter Identification," Proceedings of the AIAA Guidance, Navigation and Control Conference, AIAA, New York, 1986.

<sup>8</sup>Coppolino, R. N., "A Simultaneous Frequency Domain Technique for Estimation of Modal Parameters from Measured Data,"

Society of Automotive Engineers, Oct. 1981.

<sup>9</sup>Zhang, L., Kanda, H., Brown, D. L., and Allemang, R. J., "A Polyreference Frequency Domain Method for Modal Parameter Identification," American Society of Mechanical Engineers, Paper 85-DET-106. Sept. 1985.

106, Sept. 1985.

Craig, R. R., Jr. and Blair, M. A., "A Generalized Multi-Input, Multi-Output Modal Parameter Estimation Algorithm," AIAA Jour-

nal, Vol. 23, June 1985, pp. 931-937.

<sup>11</sup>Ho, B. L. and Kalman, R. E., "Effective Construction of Linear State-Variable Models From Input/Output Data," *Proceedings of the 3rd Annual Allerton Conference on Circuit and Systems Theory*, Univ. of Illinois, Dept. of Electrical Engineering, 1965, pp. 449–459; also,

Regelungstechnik, Vol. 14, 1966, pp. 545-548.

<sup>12</sup>Sundararajan, N. and Montgomery, R. C., "Identification of Structural Dynamics Systems Using Least-Square Lattice Filters," *Journal of Guidance, Control, and Dynamics*, Vol. 6, Sept.-Oct. 1983, pp. 374-381.

pp. 374–381.

13Gillis, J. T., Smit, G. N., and Yong, K., "Structural Identification

by Lattice Least Squares," AAS Paper 85-423, Aug. 1985.

14Rissanen, J., "Recursive Identification of Linear Systems," SIAM

Journal on Control, Vol. 9, No. 3, Aug. 1971, pp. 420–430.

15De Jong, L. S., "Numerical Aspects of Recursive Realization Al-

<sup>15</sup>De Jong, L. S., "Numerical Aspects of Recursive Realization Algorithms," *SIAM Journal on Control and Optimization*, Vol. 16, July 1978, pp. 646–659.

<sup>16</sup>Franklin, J. N., Matrix Theory, Prentice-Hall, Englewood Cliffs,

NJ, 1986.

<sup>17</sup>Klema, V. C. and Laub, A. J., "The Singular Value Decomposition: Its Computation and Some Applications," *IEEE Transactions on Automatic Control*, Vol. AC-25, No. 2, April 1980, pp. 164–176.

# June 26, 1989

# Candidates Solicited for JSR Editor-in-Chief Post

On January 1, 1990, AIAA will appoint a new Editor-in-Chief of its *Journal of Spacecraft and Rockets (JSR)*, and solicits candidates for this prestigious editorial post.

The selection committee to replace Dr. Frank J. Redd, who will be retiring from the position of Editor in Chief as of December 31, 1989, will be chaired by Earl. H. Dowell, a past Vice President – Publications. Other members of the selection committee include Allen E. Fuhs, William H. Heiser, and Paul F. Holloway. Fuhs and Heiser have also served terms as VP – Publications. To apply for the editorship, submit four copies of an application citing qualifications and your objectives for the journal to:

Prof. Earl H. Dowell c/o Norma Brennan AIAA Headquarters 370 L'Enfant Promenade, S.W. Washington, D.C. 20024-2518

The deadline for applications will be September 30, 1989.

JSR now has the following scope:

"This journal is devoted to reporting advancements in the science and technology associated with spacecraft and tactical and strategic missile systems, including subsystems, applications, missions, environmental interactions, and space sciences. The Journal publishes original archival papers disclosing significant developments in spacecraft and missile configurations, system and subsystem design and application, mission design and analysis, missile and spacecraft aerothermodynamics, space instrumentation, developments in space sciences, space processing, and manufacturing, space operations, and applications of space technologies to other fields. The context of the Journal also includes ground-support systems, manufacturing, integration and testing, launch control, recovery, and repair, space communications, and scientific data processing. Papers also are sought which describe the effects on spacecraft and missile design and performance of propulsion, guidance and control, thermal management, and structural systems."

Duties of the Editor-in-Chief encompass the following: Foreseeing and stimulating major contributions to the journal, with assistance from an Editorial Advisory Board. Logging in, acknowledging, and appraising submitted manuscripts; checking their general quality, importance to the technical community, and compliance with editorial specifications; assigning them to Associate Editors for processing; arbitrating editorial disputes; tracking manuscripts and Associate Editor actions via computer.

The post carries an honorarium of \$225 per month and reimbursement for allowable expenses up to a maximum of \$3,400 per year.

Address questions about editing procedures or other factors connected with duties to: Norma Brennan, AIAA Director, Editorial and Production Departments (202-646-7482).

Questions concerning policy may be directed to me in writing at the following address: Dr. Billy M. McCormac, AIAA Vice President – Publications, D9l-01/B256, Lockheed R&DD, 3251 Hanover Street, Palo Alto, CA 94304

B. M. M.